



FIRMAIN/CEAUCOMP: Multiphysics modeling of the hygro-mechanical behavior of composites used in Marine Renewable Energy structures

A. Clément, A. Uguen, Q. Dézulier, S. Fréour, F. Jacquemin

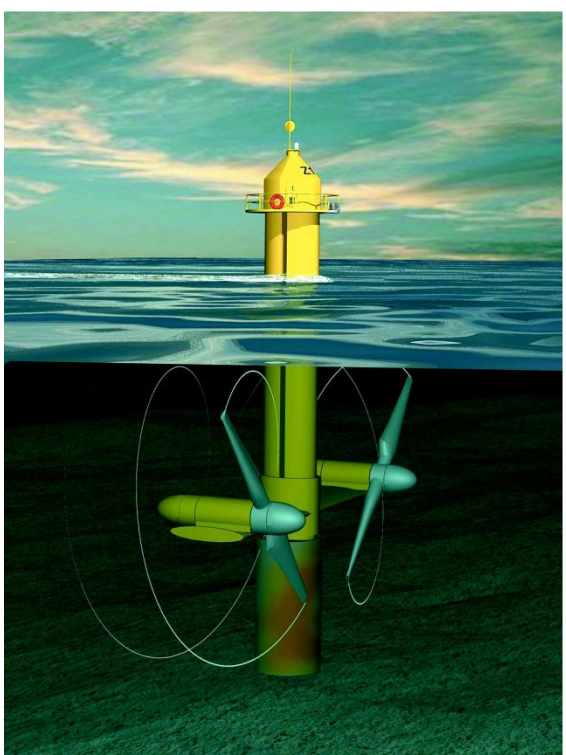
GeM, Research Institute in Civil and Mechanical Engineering, CNRS UMR 6183, Nantes University, Centrale Nantes, France

SCIENTIFIC AND INDUSTRIAL MOTIVATIONS

Composite materials used in RME structures are submitted to **harsh environments** leading to a possible moisture diffusion process. This aging may involve **relevant internal mechanical states** coupled to a significant **drop of the mechanical properties** and thus may **damage the material** and the structure.

General problem

Composite structures submitted to harsh marine environments



Complex **coupled** loadings:

- **Humidity**
- Temperature
- Chemical aggressions
- Solar radiations
- **Mechanical loadings**

Challenges:

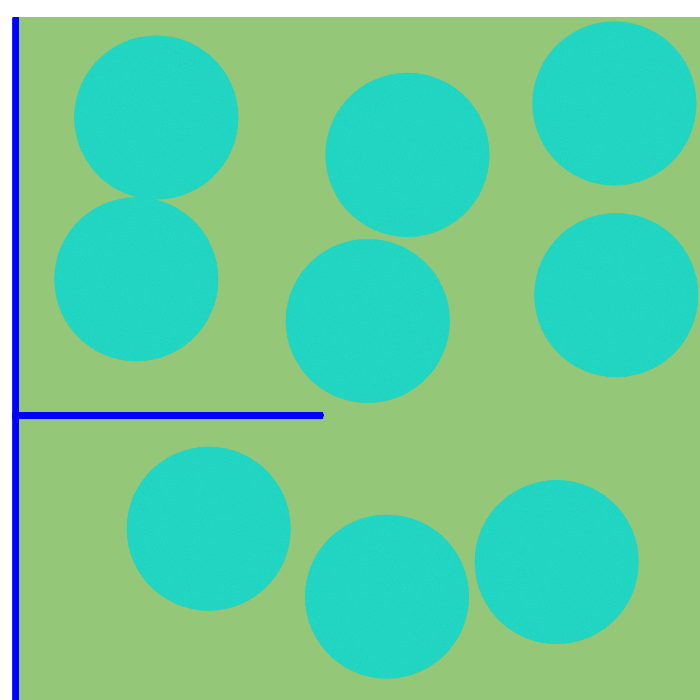
- **Good understanding** of the physical phenomena and their interactions
- Development of **efficient/predictive multiphysics** and **multiscale tools**

FIRMAIN and CEAUCOMP particular objectives

- The FIRMAIN project aims at studying the impact of hygroscopic aging on **crack propagation** submitted to **uncertainties** in composite materials using both X-FEM methodology and spectral stochastic approaches
- The CEAUCOMP project aims at developing predictive models for composites under **fully coupled conditions**, *i.e.* combined simultaneous exposure of the composite to immersion in water or humid air while being subjected to mechanical loading

FIRMAIN PROJECT (2016-2019)

Heterogeneous Fick diffusion problem



Find $c(\mathbf{x}, t) \in \Omega \times \mathbb{R}_+^+$ such that

$$\frac{\partial c(\mathbf{x}, t)}{\partial t} = \mathbf{D} \Delta c(\mathbf{x}, t) \quad \text{in } \Omega \times \mathbb{R}_+^+$$

$$c(\mathbf{x}, t) = c^\infty \quad \text{on } \Gamma_1 \times \mathbb{R}_+^+$$

$$(\mathbf{D} \nabla_x c(\mathbf{x}, t)) \cdot \mathbf{n} = 0 \quad \text{on } \Gamma \setminus \Gamma_1 \times \mathbb{R}_+^+$$

$$c(\mathbf{x}, t=0) = c_0(\mathbf{x}) \quad \forall \mathbf{x} \in \Omega$$

where $\Omega = \Omega_1 \cup \Omega_2$ and $\mathbf{D} = \begin{cases} \mathbf{D}_1 & \text{if } \mathbf{x} \in \Omega_1 \\ \mathbf{0} & \text{if } \mathbf{x} \in \Omega_2 \end{cases}$

eXtended Finite Element methodology

- **Implicit** description of the geometry with **level-sets**
- **Enriched approximation** based on prior physical knowledge [Moës et al. 1999]

Use of a **penalty approach** for Dirichlet BC along the crack

$$(\mathbf{K} + \gamma \mathbf{K}^p) \mathbf{u} = \gamma \mathbf{f}^p \quad \text{where } \mathbf{K}^p = \int_{\Gamma_{crack}} N_i N_j d\Gamma \quad \text{and } \mathbf{f}^p = \int_{\Gamma_{crack}} N_i C_{imp} d\Gamma$$

Enriched approximation to represent **irregularities**

$$c(\mathbf{x}) = \sum_i N_i(\mathbf{x}) c_i + \sum_i N_i(\mathbf{x}) H(\mathbf{x}) c_i^+$$

where $H(\mathbf{x})$ is the Heaviside function based on the sign of the level set values

Spectral stochastic approach

- **Uncertainties** propagation with Polynomial Chaos expansion

Decomposition of the solution on a specific basis

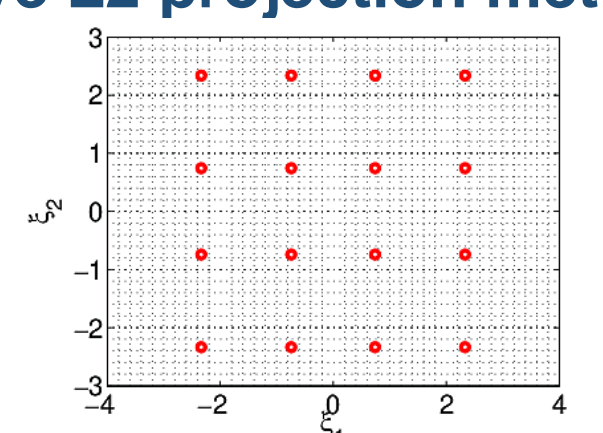
$$c(\mathbf{y}, \xi) \approx \sum_{\alpha=1}^P c_\alpha(\mathbf{y}) H_\alpha(\xi)$$

where the $c_\alpha(\mathbf{y})$ are the **unknown** of the problem and the $\{H_\alpha\}_{\alpha=1}^P \in L^2(\Xi, dP_\xi)$ is a basis of **orthonormal polynomials** choosing with respect to the density of probability P_Ξ (Polynomial Chaos [Ghanem et al. 1991, Xiu et al. 2002])

Computation with a non-intrusive L2 projection method

$$c_\alpha = E(c H_\alpha) = \int_{\Theta} H_\alpha(\xi) c(\xi) dP_\xi$$

$$c_\alpha \approx \sum_{k=1}^{n_g} \omega_k H_\alpha(\xi_k) c(\xi_k)$$



Microscale numerical study

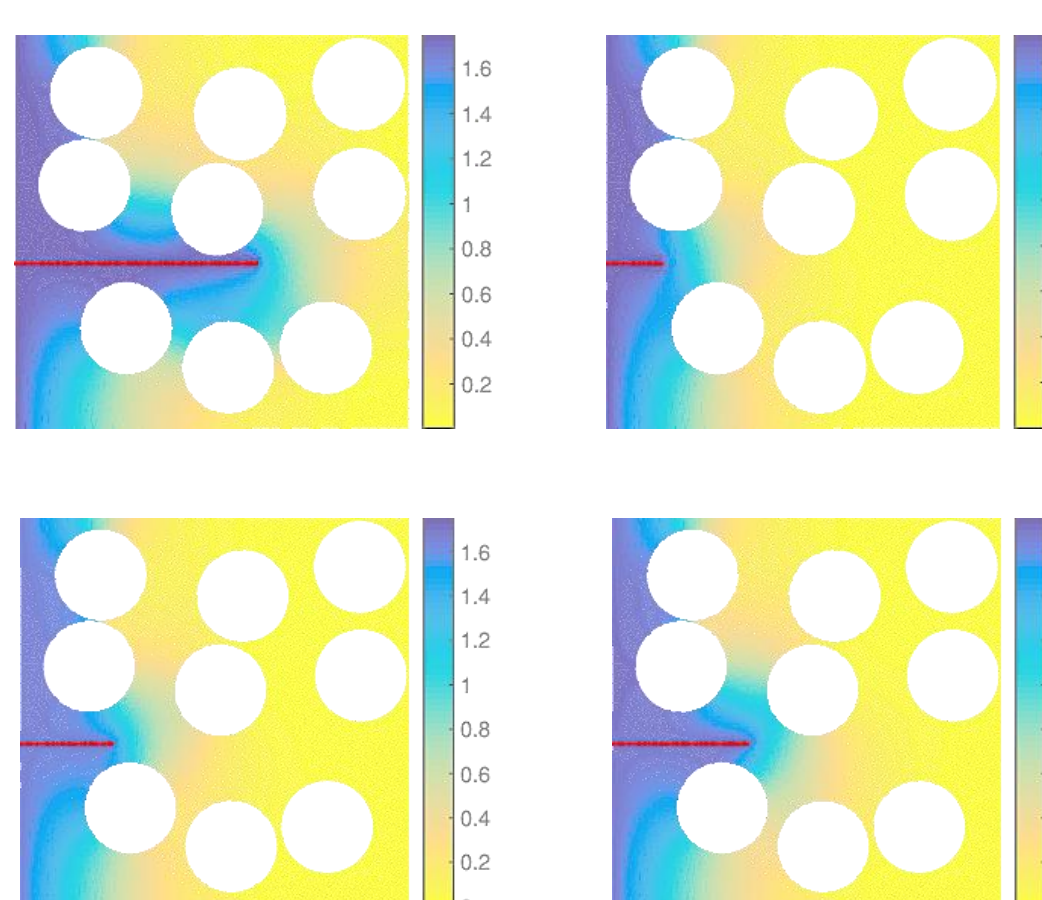
Problem description:

- **Random crack length** L_{crack} in $U(5, 45) \mu\text{m}$
- **Random imposed C^∞** in $U(1.5, 1.9) \% \text{H}_2\text{O}$
- Isotropic moisture coefficient $D = 8.2 \cdot 10^{-2} \mu\text{m}^2/\text{s}$
- Volume fraction $v_f = 40\%$ with $d_f = 10 \mu\text{m}$

Approximation parameters :

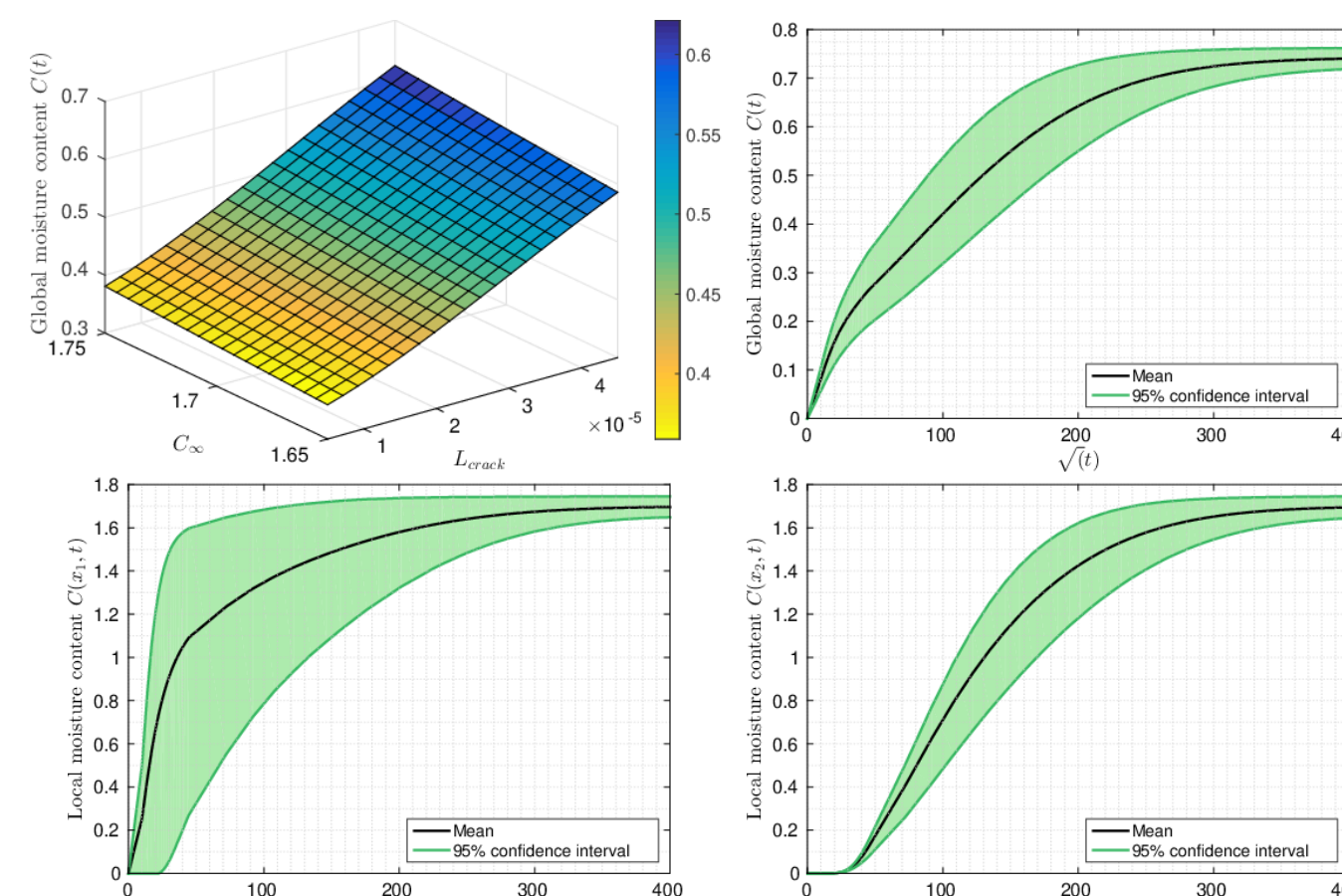
- Mesh with 7200 linear finite elements
- Euler's implicit scheme for $T = 45 \text{ h}$ with $\Delta t = 100 \text{ s}$
- **Penalty parameter** $\gamma = 10^6$
- **Stochastic approximation** with $p = 3$

Random realizations of moisture field



Fast post-processing of the stochastic solution

Results on global and local moisture content



Relevant influence of the crack on both quantities

Ongoing work and perspectives

Ongoing work:

- Implementation of the **mechanical problem** within the X-FEM framework (crack propagation)
- Determination of **effective/apparent** properties
- Numerical studies at mesoscopic and macroscopic scales
- **Experimental campaign** on Glass/epoxy composite

Perspectives:

- Introduction of **local dependencies** for mechanical properties (hygro-mechanical coupled problem)
- Extension to other composite damage processes such as **debonding** and **delamination**

CEAUCOMP PROJECT (2018-2021)

Experimental campaign

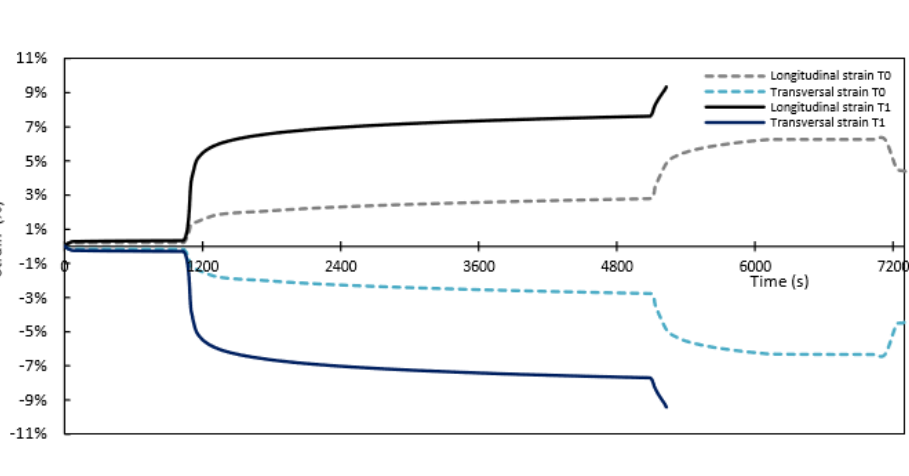
Objective: carry out specific **coupled creep test** in immersion and humid environments



- Development of a **specific device**
- Use of dedicated **obround shaped** samples to avoid the use of conventional clamping jaws



Obround shaped samples

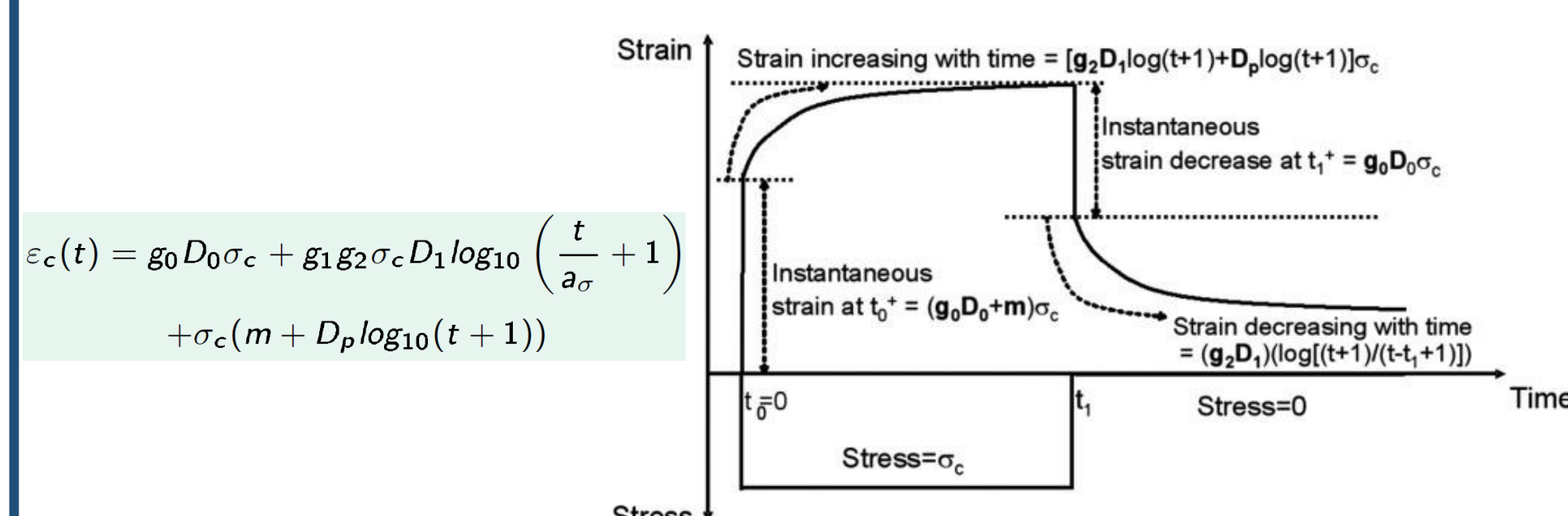


Creep response before and after aging

Coupled hygro-mechanical modeling

Objective: modeling of the **visco-elastic behavior during aging**

Implementation of dedicated coupled models with moisture diffusion such as [Derombise et al., 2011]



Perspectives

- Taking into account the various sources of **uncertainties**
- Adding the possible existence of **defects** within the material
- Extension of the model to the **thermal** behavior

References

- Ghanem R. and Spanos P. Stochastic finite elements: a spectral approach, Springer, Berlin, 1991.
- Xiu D. B. and Karniadakis G. E. The Wiener-Askey polynomial chaos for stochastic differential equations, SIAM J. Sci. Comput., 24(2):619-644, 2002.
- Moës N., Dolbow J. and Belytschko T. A finite element method for crack growth without remeshing, IJNME, 46:131-150, 1999.
- Derombise G., Chailleux E., Forest B., Riou L., Lacotte N., Vouyovitch L., Davies P. Long-term mechanical behavior of aramid fibers in seawater, Polymer Engineering and Science, 51(7):1366-1375, 2011.